The Three-Line Stereo Camera MEOSS and its Application in Space

F. Lanzl DFVLR, German Aerospace Establishment Institute for Optoelectronics D-8031 Oberpfaffenhofen, FRG

1. INTRODUCTION

In 1980 the Indian Space Research Organization ISRO offered to DFVLR to fly an experiment of 10-20 kg on a Stretched ROHINI Satellite (SROSS) of the 150 kg class.

The common understanding is to fly under the constraints of the SROSS mission (Table 1) an attractive low cost experiment provided by DFVLR.

Table 1: Nominal specifications for SROSS-MEOSS Mission

Mission Parameters

circular orbit inclination orbital period lifetime launch telemetry data rate payload weight payload power 450 km 45.56° (48.20°) 92.8 minutes 6-12 months 1988 S-band 10.4 Mbit 10 kg 25 Watt for 20 minutes/day

2. THE INSTRUMENT

The main characteristics of the proposed threefold stereoscopic CCD line scan camera are:

- a single objective (monocular) imaging system for reduction of weight and adjustment efforts
- no moving mechanism
- passive cooling
- three relatively long CCD lines of 3456 pixels in one common focal plane
- one spectral band between 570 to 700 nm
- 8 bit radiometric resolution
- LANDSAT MSS compatible geometrical resolution
- correction for earth rotation by electronic shift.

The optomechanical design with a central, mechanically independent imaging unit consists of a space modification of a Zeiss Biogon objective and the focal plane containing three parallel CCD lines vertical to flight direction as shown in Fig. 1. The central CCD line contains the optical axis and produces the nadir looking image, while the outer lines see the same parts of a scene at different angles and times (fore and aft looking images). A baffle shields the objective from straylight. To reduce deforming effects from temperature differences the central case is fabricated from Titanium. The overall weight of the camera is 6.5 kg.



Fig. 1 Shows the vital parts of the MEOSS camera: space modified ZEISS BIOGON objective, 3 CCD's mounted in the focal plane, the electronics necessary to register and transform signals collected by the CCD's. The instrument characteristics are summarized in

Table 2:

Camera Data:

ZEISS Biogon optics 61.1 mm focal length $\Delta y = 10.7 \ \mu m$ n = 3456 IFOV = 0.01° square distance of elements on CCD number of elements on CCD instantaneous field of view d = 26.69 mmB = $\pm 23.60^{\circ}$ f = 131.1 Hzdistance of scanlines convergence angle scanline frequency spectral channel 570-720 nm

3. MISSION

The image data reception is performed by the ISRO-NRSA LANDSAT ground station near Hyderabad and by the DFVLR ground station Weilheim and is open to other ground stations within the mission constraints.

Fig. 2 shows the ground tracks for both stations

Fig. 3 for Weilheim in detail.

The received image data are determined by the following mission characteristics data.

Table 3:

Orbit Data:

height Includen = 450 kmground track velocityV = 7.137 km/sinclinationi = 45.60° (48.20°)sinodal period of orbital drift24 hours in 55.6 daysvisibility range at Weilheim1730 km at 5° elevationNo. of observable successive orbits4 to 5

h = 450 km



The diagram displays the ground tracks for the MEOSS-SROSS-2 mission for 1 day. An altitude H = 450 km and an inclination of 45.6 ° is assumed. Shown are the visibility circles of Weilheim and Hyderabad for 5 ° and 10 ° satellite elevation. An orbit inclination of 48.2 ° is under consideration.

Fig. 2



Fig. 3 Weilheim receiving station. Example for 5 consecutive orbits (numbers 1 through 5) respresenting the coverage of one day. The swath width marked by parallel lines is 255 km. Dotted lines mark the range of the station for an elevation of the satellite above the horizon of 5° respectively 10°. Because the pattern of passes is shifting 6.5° eastwards a day, full coverage of the area shown, can be achieved within 6 days.

Table 4:

Performance Data:

8 bit radiometric resolution selectable gain factors 1,2 and 4= 78.8 mground pixel along scanline Ρ = 52.0 minter scanline distance Ρ Ρ = 54.7 mheight resolution element swath width (central CCD) SW = 255.8 kmbaselength (nadir track) corr. time interval (nadir track) BL = 396.1 and 2x198 km = 58.1 and 2x29.5 sec t ß° $= \pm 25.41^{\circ}$ and 0° ground based convergence angle B:H = 0.950 and 2x0.452effective base to height ratio active pixels per scanline n = 3237 $\Delta v = 1.12 \text{ and } 2.24 \text{ m/s}$ resolution for cross track wind $\Delta h = 61.1 \text{ and } 122.2 \text{ m}$ height error for 1 m/s along track wind

Image data evaluation is done in two steps

preprocessing radiometric calibration earth rotation and curvature correction orbit and attitude correction

high precission correction using threefold stereo information redundancy attitude modelling

The preprocessed data are available to all users. A high precission correction scheme is also built up and further dealt with in the next chapter under "Photogrammetric Image Correction and Evaluation".

4. SCIENTIFIC OBJECTIVES

The main goals of the MEOSS mission are

- generation of threefold stereoscopic linescanimagery from space
- investigation of procedures for image rectification
- investigation of correlation accuracies over land and cloud fields

with the following derived products

- rectified linescan images and stereo triplets
 1 : 1 000 000 scale
- orthophotos and ortho-stereo triplets
 1 : 500 000 scale
- heights and cross-track velocties of cloud fields.

Meoss will be the first stereo scanner in space and offers the possibilities of

- basic investigation and test of different evaluation methods for threefold stereo scan systems and by this experience for the plannung of future higher resolution systems
- incorporation of orbit and attitude data of the satellite for the evaluation of the stereo information.

The program scheme to achieve these goals is indicated in Fig. 4.



Fig. 4 MEOSS HIGH PRECISION CORRECTION SCHEME

Geometric image correction will be based on ground control points and a large number of conjugate points, representing identical location in the three corresponding image stripes. In addition satellite orbit and attitude data are introduced. The result of these calculations involving photogrammetric collinearity equations are the position and orientation parameters of each recorded line, which can be applied to correct the image data.

In the following the type and magnitude of attitude variations of the satellite which cause a different orientation for each recorded line are given in more detail. Fig. 5 shows the attitude relevant aspects of the satellite schematically. Table 5 gives the attitude characteristics, table 6 and 7 the resulting dynamic image distortions and the static image displacement. Table 8 sumarizes the planned results of the indicated correction procedure.





Attitude Behavior of SROSS - 02 Satellite

Table 5 ATTITUDE CHARACTERISTICS OF SBOGS-02 SATELLITE

	roll	pitch	yaw
Conical Scan Earth Sensor			
resolution	0.15*	0.15°	(0.4°)
Pitch Control System			
control range	an an an	+ 2.5° ± 0.5°	ab 68 68
random drift	en m aj	± 0.1°	40 60
drift periods	88 87 ap	≥ 50 sec	
drift frequencies	60 G C	$\leq 2 \cdot 10^{-2}$ Hz	80 80 6 0
Roll and Yaw Control Syst	88		
Control range	<u>+</u> 1.5°		± 3°
drift period	~ 5000 sec	400 tille 400	~ 5000 860
drift frequency	~ 2 · 10 Hz		~. 2 · 10 Hz
Nutation			
drift range	± 0.05°	an es en	± 0.03°
drift period	~ 12.5 sec	anga data data .	~ 12.5 sec
drift frequency	$-8 \cdot 10^{-2}$ Hz	au ao 40	~ 8 · 10 ⁻² Hz

I-192

Table 6 Dynamic Image Distortion

Pitch random drift

 \pm 0.1° $\hat{-}$ \pm 15 pixel shift along X-axis period > 50 sec; scene duration 29 sec

Nutation

 \pm 0.05° \simeq \pm 7 pixel shear between Y-axis and X/Z-axis period \sim 12.5 sec, scene duration 29 sec

T<u>able 7</u>

Image Displacement

Tracking Error 0.4 - 2 km ² 8 - 40 pixel absolute position along X-axis

Earth Rotation (latitude dependent, electronically compensated) \pm 8.6 km $\hat{-} \pm$ 110 pixel lateral displacement of fore and aft direction lines

Control system offset

pitch $2.5^{\circ} \pm 0.5^{\circ} \stackrel{-}{\rightarrow} 375 \pm 75$ pixel shift and scale change along X-axis

roll $\pm 1.5^{\circ} - \pm 150$ pixel shift and scale change along Y-axis

yaw $\pm 3^{\circ} - \pm 450$ pixel shear between X- and Y-axis Table 8

<u>Correction of</u> <u>Image Distortion and Image Displacement</u>

1 MEOSS pixel

IFOV = 0,01° -
$$P_{y}$$
 = 79 m; P_{x} = 52 m

1 MEOSS scene

swath width SW = 256 km² 3237 pixel, SW : H = 0,566 basis (length) $B = \pm 198 \text{ km}^2 \pm 3800 \text{ pixel}, B : H = \pm 0.452$

Goal of correction:

better than 0,03° - 3 pixel

Data of MEOSS will be of importance for the following fields of application.

Cartographic Applications Α.

Suggested activities are:

- registration of stereo images to a standard grid system
- derivation of ortho photos and ortho stereo triplets resampling procedures
- experimental derivation of topographic and orthophoto maps on scales 1:500 000 and eventually 1:250 000
- revision of topographical maps up to a scale 1:150 000.
- B. Applications in Geology, Forestry, and Environmental Sciences

Suggested applications are:

- correlation of MEOSS stereo data with LANDSAT MSS, TM or SPOT multispectral data
- geolocigal mapping (lithology and structures) studies on angular variations of radiances; discrimination between surface and atmospheric effects
- forest inventory
- land use inventory.

In performing these tasks two features of the MEOSS mission may be of special interest:

- varying illumination (approx. 26 min. time shift per day)
- nearly 90° difference of stereoscopic viewing direction for observation from ascending and descending orbit segment at low latitudes.

C. <u>Meteorology</u>

The following information could be derived:

- 1. From MEOSS data alone
 - cloud classification by 3 dimensinal observation at high resolution
 - cloud-snow discrimination
 - discrimination of Cirrus against diffuse background as dense cloud fields, snow covered areas and turbity patterns in water bodies
 - cross track cloud velocities with 1.2 m/s resolution
 - estimate of sea state from sunglint, detectable at three differently inclined scan planes
 - estimation of cloud field dynamics by stereo observation from successive orbits with 93 min. time gap.
- 2. From combination with other data sources
 - true heights of clouds and clouds displacement vectors by stereoscopy (along track cloud displacement velocity required. 1 m/s error leads to 61.1 m error in height assigment)
 - optical density of clouds (radiation temperatures required).