

## NM3digit: the DLT algorithm in a digital photogrammetrical software for the survey teaching

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### Abstract

Often in the photogrammetrical survey teaching there are some difficulties in the organization of the exercises of students. This is connected to the insufficient number of instruments used in the restitution compared to the high number of students. Starting from this consideration the authors have realized a software in win95 environment that allows the orientation and the restitution of non-metric photograms digitalized using the D.L.T. algorithms. The paper explains the reasons of the choice of the algorithm, of the digital environment, of the operative system, of the programming language, etc. It is proposed to create a Web site for the distribution of free-software for photogrammetry and topography. The software presented in this paper is given as compiled and source code.

### Introduction

Within the field of the activities done by the Photogrammetrical Laboratory of IUAV, the work presented here is born from a simple idea: it is impossible to place the instruments of photogrammetrical restitution at the disposition of the students of the Survey courses and the graduands who need to use them for their theses. This is due to the large number of students compared with the limited number of restitution systems. In the past, the problem was overcome by the organization of the technical personnel who afforded students the opportunity to take part in demonstrations of the instruments without actual first hand experience in the operations that they have studied on a theoretical basis.

A real understanding of the relative problems of the "instrumental survey" involves not only dealing with the theoretical aspects and methodologies but practical and operative ones as well, which can be acquired only through a real application.

This new need for a direct experience in the teaching of operative survey stems probably from two factors: firstly, from the more and more precise definition of the architectonic survey discipline which has brought about, among other things, the individuation of the methods of transmission of the disciplinary knowledge (of which this symposium is proof). Secondly, the understanding of the importance of survey within the field of conservation on the understanding and knowledge of an architecture, which brings about a rigour in the methods that can be guaranteed only by operators with a complete and deep rooted training. The objective placed therefore, has been plotting the photogrammetrical restitution accessible to a large

number of students, taking advantage of the possibilities offered by present day computers.

This end is reached through the realization of a photogrammetrical system which utilizes low cost hardware such as personal computers and non metric cameras, tools easily accessible and useable by all students.

The software must allow for the use of non-stereoscopic and non-metric images, maintaining the rigorousness of the operation of orientation and restitution.

The software realized cannot be considered a digital photogrammetrical system, in so far as it doesn't have any of the fundamental technical characteristics, but it is nearly revolutionary in the production and the utilization of the photogrammetrical products, which will be shown herein. The diffusion of soft-photogrammetry will bring the end-user to be not only the consumer and user of the maps produced by photogrammetry, but he will also be able to produce for himself maps containing all the specific data necessary to his particular project.

In the same way the student can perform the operations of orientation, restitution, evaluation of the estimates of the parameters obtained, and uncertainty of the points surveyed himself.

With the software NM3-Digit, it will not only be possible to change the way in which the exercises in the Survey and Photogrammetrical courses are carried out, but also change the service offered by the Photogrammetrical Laboratory with respect to the student. Up until now, the student received a final product from the Laboratory: a survey or a demonstration of how to execute a survey; with software instruments such as NM3-Digit, available with the freeware formula in so far as they are self produced,

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it will be possible to hand over to the student the software, the photographs and the control points relative to the photographs (and eventually also the orientation). In this way, the student can perform the orientation and the restitution, personally appraising what to plot and how to plot it.

### Basic Decisions

In relationship to what is described, the NM3-Digit software must have precise characteristics:

- to allow for the restitution with non-metrical camera;
- to work with PC s and under the Windows operating system.

The choice of the algorithm of the calculation has been decided to be the D.L.T. for its characteristics of the treatment of non-metrical images. Moreover, the D.L.T. is an expression of the projective relationships between two-dimensional space and three-dimensional space, which, being considered the basis of photogrammetry, have great teaching value.

The monoscopy has been another obligatory choice in so far as it eliminates any optical hardware components.

It has been decided not to supply the product with a graphic output, but rather only a numerical output, interfacing it *on line* with CAD.

Another fundamental decision is that of showing all the calculated parameters and the imposing the obligation to manually update the results of every repetition; this slows down the operations but allows the student to evaluate the results and to make the consequential decisions.

### What it does and doesn't do

The photogrammetric workstation is characterized by notable services, above all in relation to the automation of certain photogrammetrical procedures;

These essentially allow for the following:

- the visualization of images
- the normalization of images
- the stereoscopic vision
- a high level of automation of the orientation procedures
- the traditional stereoscopic or the monoscopic restitution
- the matching of images
- the automatic generation of D.T.M. and contour lines
- the monoscopic or three-dimensional superimposition
- orthophotos

A system of this kind does not work with a *Personal Computer*, but rather with a computer dedicated, developed and designed by the companies that produce photogrammetrical *Hardware*.

The NM3-Digit software permits some of the aforementioned operations to be carried out, which constitute the minimum operative basis and the starting point for successive developments.

In particular, it permits:

- the reading and visualization of images;
- the reading from the monitor of the coordinate images (pixel);
- the spatial resection:
  - with direct solution (11 parameters of the D.L.T.)
  - with iterative solution (11 parameters of the D.L.T. + 1 parameter that models the radial distortion);
- the spatial intersection for multi-image restitution;
- the evaluation of statistical parameters;
- the saving of the parameters for successive restitutions

Therefore the digital photogrammetric system cannot be defined according to currently used definitions but rather it is simply a photogrammetric system on the PC that utilizes digital images.

### D.L.T.

The Direct Linear Transformation (D.L.T.) is an alternative method for facing the problem of analytical orientation that finds an optimal application in photogrammetry with non metrical images.

The main advantages are represented by the fact that with this method a stable interior orientation nor fiducial marks are necessary. In the initial phase of the calculation moreover, it is not necessary to know the approximate values for the unknown parameters.

The solution with D.L.T. is based on the concept of the direct transformation of coordinates in the instrumental system of the comparator of the coordinate object. The intermediate passage from comparator coordinate to image coordinate is latent in the D.L.T. equations and is not calculated explicitly.

The functional tie between the object coordinates and the image coordinates is given by 11 parameters. The geometric significance of the parameters of the D.L.T. is clear: they are combinations of the three parameters of interior orientation ( $x_0, y_0, c$ ) and of the 6 of external orientation ( $X_0, Y_0, Z_0, \omega, \phi, \kappa$ ) of a photogram.

The other two parameters of the D.L.T. compared with the 9 parameters of the photogram can be interpreted as:

- a different scale in x and y axes (m);
- a shear (=orthogonality error) between x and y axes ( $\beta$ ).

These measures can be interpreted as a affine transformation applied to the image.

These two conditions can be utilized for the writing of the two equations between the parameters of the D.L.T. if the values of m and  $\beta$  are known (for example, utilizing numbered metrical images with a



photogrammetric scanner for which  $m=1$  and  $\beta=0$ ) and can also be used for modeling the errors of the comparator. In the case of the NM3-Digit, with which one must use low cost hardware tools, the two extra parameters are used to model the deformations introduced by the scanner which constitutes the comparator. The deformations are simplified into:

- difference of scale along the x and y axes due to the fact that one direction of the scanner the coordinates are determined by the steps of the movement of the motor of the optical group;
- the non-orthogonality of the axes due to the placement of the sensors in respect to the direction of the movement.

It seems that in utilizing non-metrical images and a low cost scanner the presence of errors in the geometry of the image necessitates the use of all 11 parameters (including, therefore, the affine transformation) to avoid running the risk of excessive numbers of parameters.

The projective relationship between the two dimensional space of the image and the three-dimensional space is described by the formula:

$$u = AU$$

where

$u$  represents the vector  $\begin{vmatrix} u & v & t \end{vmatrix}^t$ ,  $A$  the matrix coefficient e  $U$  the vector  $\begin{vmatrix} U & V & W & T \end{vmatrix}^t$ .

$$\begin{vmatrix} u \\ v \\ t \end{vmatrix} = \begin{vmatrix} a_1 & a_2 & a_3 & a_4 \\ a_5 & a_6 & a_7 & a_8 \\ a_9 & a_{10} & a_{11} & a_{12} \end{vmatrix} \cdot \begin{vmatrix} U \\ V \\ W \\ T \end{vmatrix}$$

With reference to the two systems of Cartesian coordinates  $(x, y)$  e  $(X, Y, Z)$  the above written relationships become

$$x = kBX$$

$$\begin{vmatrix} x \\ y \\ 1 \end{vmatrix} = k \cdot \begin{vmatrix} b_1 & b_2 & b_3 & b_4 \\ b_5 & b_6 & b_7 & b_8 \\ b_9 & b_{10} & b_{11} & 1 \end{vmatrix} \cdot \begin{vmatrix} X \\ Y \\ Z \\ 1 \end{vmatrix} \quad [1]$$

having placed:

$$\frac{u}{t} = x; \quad \frac{v}{t} = y; \quad b_j = \frac{a_j}{a_{12}} \left( b_{12} = \frac{a_{12}}{a_{12}} = 1 \right);$$

$$k = \frac{T}{t} a_{12}; \quad X = \frac{U}{T}; \quad Y = \frac{V}{T}; \quad Z = \frac{W}{T}$$

Each of the vectors is assigned an index of identification  $i$  to the  $n$ th of the image or object point

$$x_i = k_i BX_i$$

Developing the [1] achieves

$$\begin{vmatrix} x_i \\ y_i \\ 1 \end{vmatrix} = \begin{vmatrix} k_i b_1 X_i + k_i b_2 Y_i + k_i b_3 Z_i + k_i b_4 \\ k_i b_5 X_i + k_i b_6 Y_i + k_i b_7 Z_i + k_i b_8 \\ k_i b_9 X_i + k_i b_{10} Y_i + k_i b_{11} Z_i + k_i \end{vmatrix}$$

Dividing the first two equations by the third achieves:

$$\begin{aligned} \frac{x_i}{1} &= \frac{b_1 X_i + b_2 Y_i + b_3 Z_i + b_4}{b_9 X_i + b_{10} Y_i + b_{11} Z_i + 1} \\ \frac{y_i}{1} &= \frac{b_5 X_i + b_6 Y_i + b_7 Z_i + b_8}{b_9 X_i + b_{10} Y_i + b_{11} Z_i + 1} \end{aligned} \quad [2]$$

These relationships put in relation the image coordinates with the object coordinates through the  $b_j$ .

#### Orientation

Now considering simultaneously the implicit transformation of the system coordinates of the comparator to that of the image and the correction of the systematic errors, the collinear equations can be expressed as follows:

$$x - d_x = x_0 + c_x \frac{m_{11}(X - Xc) + m_{12}(Y - Yc) + m_{13}(Z - Zc)}{m_{31}(X - Xc) + m_{32}(Y - Yc) + m_{33}(Z - Zc)}$$

$$y - d_y = y_0 +$$

$$c_y \frac{m_{21}(X - Xc) + m_{22}(Y - Yc) + m_{23}(Z - Zc)}{m_{31}(X - Xc) + m_{32}(Y - Yc) + m_{33}(Z - Zc)}$$

where the  $x$  and  $y$  are image coordinates of a point in the system defined by the comparator,  $d_x$  e  $d_y$  are the systematic errors of the image coordinates,  $x_0$  e  $y_0$  are the coordinates of the principle points in the comparator system, and  $c_x$  e  $c_y$  are the principle distances along the  $x$  and  $y$  directions. The difference between the major distance along the  $x$  and  $y$  directions is given by the different variation of the scale assumed in the affine transformation of the coordinates from the comparator system to the object one.

Having placed:

$$L_1 = \frac{x_0 m_{31} + c_x m_{11}}{L}$$

$$L_2 = \frac{x_0 m_{32} + c_x m_{12}}{L}$$

$$L_3 = \frac{x_0 m_{33} + c_x m_{13}}{L}$$

$$L_4 = x_0 + \frac{m_{11} X_c + m_{12} Y_c + m_{13} Z_c}{L}$$

$$L_5 = \frac{y_0 m_{31} + c_y m_{21}}{L}$$

$$L_6 = \frac{y_0 m_{32} + c_y m_{22}}{L}$$

$$L_7 = \frac{y_0 m_{33} + c_y m_{23}}{L}$$

$$L_8 = y_0 + \frac{m_{21} X_c + m_{22} Y_c + m_{23} Z_c}{L}$$

$$L_9 = \frac{m_{31}}{L}$$

$$L_{10} = \frac{m_{32}}{L}$$

$$L_{11} = \frac{m_{33}}{L}$$

$$L = -(m_{31} X_c + m_{22} Y_c + m_{13} Z_c)$$

with some algebraic passages the following equations are obtained:

$$x - d_x = \frac{L_1 X + L_2 Y + L_3 Z + L_4}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

$$y - d_y = \frac{L_5 X + L_6 Y + L_7 Z + L_8}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

Subtracting  $d_x$  e  $d_y$  e and substituting the symbol "b" with "L" the equations [3] are identical as those of [2].

The  $d_x$  e  $d_y$  terms can be written explicitly, the [3] equations become:

$$x + (x - x_0)(K_1 r^2 + K_2 r^4 + K_3 r^6 + \dots) + [r^2 + 2(x - x_0)^2] P_1 + 2(y - y_0)(x - x_0) P_2 = \frac{L_1 X + L_2 Y + L_3 Z + L_4}{L_9 X + L_{10} Y + L_{11} Z + 1};$$

$$y + (y - y_0)(K_1 r^2 + K_2 r^4 + K_3 r^6 + \dots) + 2(y - y_0)(x - x_0) P_1 + [r^2 + 2(y - y_0)^2] P_2 = \frac{L_5 X + L_6 Y + L_7 Z + L_8}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

where  $r^2 = (x^2 + y^2)$ ;  $K_1, K_2, K_3, P_1$  e  $P_2$  are the coefficients of distortion of the objective system; X, Y, Z are the object-coordinates of the represented point;  $L_1 \dots L_{11}$  are the 11 unknown coefficients of transformation.

On the basis of experimental research, it has been concluded that, as a practical end, in order to significantly correct the distortion of the lenses, only the  $K_1$  term need be taken into consideration.

Therefore:

$$x + x' K_1 r^2 = \frac{L_1 X + L_2 Y + L_3 Z + L_4}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

$$y + y' K_1 r^2 = \frac{L_5 X + L_6 Y + L_7 Z + L_8}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

### Direct solution

The equations of the D.L.T. become the following when the terms of the distortion and the residuals of the observed points (the image coordinates) are not considered:

$$x = \frac{L_1 \cdot X + L_2 \cdot Y + L_3 \cdot Z + L_4}{L_9 \cdot X + L_{10} \cdot Y + L_{11} \cdot Z + 1}$$

$$y = \frac{L_5 \cdot X + L_6 \cdot Y + L_7 \cdot Z + L_8}{L_9 \cdot X + L_{10} \cdot Y + L_{11} \cdot Z + 1}$$

Writing the equations for unknown n points obtains a system of 2n equations in 11 unknowns; if the  $n > 6$  then the parameters of the D.L.T. can be estimated applying the method of the least squares.

In fact, for every point to the  $i$ -*nth* degree, the equations of the D.L.T. can be written in the form:

$$L_1 X_i + L_2 Y_i + L_3 Z_i + L_4 - x_i X_i L_9 - x_i Y_i L_{10} - x_i Z_i L_{11} = x_i$$

$$L_5 X_i + L_6 Y_i + L_7 Z_i + L_8 - y_i X_i L_9 - y_i Y_i L_{10} - y_i Z_i L_{11} = y_i$$

or in matrix form

$$\begin{bmatrix} L_1 \\ L_2 \\ L_3 \\ L_4 \\ L_5 \\ L_6 \\ L_7 \\ L_8 \\ L_9 \\ L_{10} \\ L_{11} \end{bmatrix} = \begin{bmatrix} X_i \\ Y_i \\ Z_i \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ -x_i \cdot X_i \\ -x_i \cdot Y_i \\ -x_i \cdot Z_i \\ 0 \\ 0 \\ 0 \\ 0 \\ X_i \\ Y_i \\ Z_i \\ 1 \\ -y_i \cdot X_i \\ -y_i \cdot Y_i \\ -y_i \cdot Z_i \\ 0 \\ 0 \\ 0 \\ 0 \\ X_i \\ Y_i \\ Z_i \\ 1 \\ -y_i \cdot X_i \\ -y_i \cdot Y_i \\ -y_i \cdot Z_i \end{bmatrix}$$

derived from the equation [4] neglecting the effect of  $v_x$  e  $v_y$  on the parameters of the distortion of the lens,  $K_1$ .

$$\begin{aligned}
 & x_i \cdot \left[ \frac{X}{A} L_1 - \frac{Y}{A} L_2 - \frac{Z}{A} L_3 - \frac{1}{A} L_4 + \frac{xX}{A} L_9 + \frac{xy}{A} L_{10} + \frac{xZ}{A} L_{11} + x'r^2 K_1 + \frac{x}{A} \right] = 0; \\
 & y_i \cdot \left[ \frac{X}{A} L_5 - \frac{Y}{A} L_6 - \frac{Z}{A} L_7 - \frac{1}{A} L_8 + \frac{yX}{A} L_9 + \frac{yY}{A} L_{10} + \frac{yZ}{A} L_{11} + y'r^2 K_1 + \frac{y}{A} \right] = 0
 \end{aligned}$$

If the 6 points of the known coordinates are considered, therefore, errors notwithstanding, it is then possible to determine with only one repeat the 11 unknown parameters of the D.L.T.

The direct solution is not very precise because the hypothesis is made that the residuals of the observation equations (image coordinates) can be neglected; it is, however, an very important solution because it allows for obtaining approximate parameters of orientation, to use after which in the *linearization* of the collinear equations.

This solution is calculated in the program and is then defined as an approximate solution.

#### Iterative solution

Considering  $v_x$  e  $v_y$ , random errors in the image coordinates measured the following expressions can be

$$\begin{aligned}
 L &= \frac{-1}{\sqrt{(L_9^2 + L_{10}^2 + L_{11}^2)}} \\
 x_0 &= (L_1 L_9 + L_2 L_{10} + L_3 L_{11}) L^2 \\
 y_0 &= (L_5 L_9 + L_6 L_{10} + L_7 L_{11}) L^2 \\
 c_x &= \sqrt{[(L_1^2 + L_2^2 + L_3^2) L^2 - x_0^2]} \\
 c_y &= \sqrt{[(L_5^2 + L_6^2 + L_7^2) L^2 - y_0^2]} \\
 \phi &= \sin^{-1} (L_9 L)
 \end{aligned}$$

Once the transformation coefficients and the error correction for all of the photographs has been obtained, the coordinates can then be estimated in the object-space in any other point that is represented in two or more photographs.

in which  $A = L_9 X + L_{10} Y + L_{11} Z + 1$ .

From the point in which the equations [5] are not linear, it is necessary in the first place to linearize them with using the Taylor's series expansion in and around the approximate values, and consequentially the solution to the least squares will have to have recourse to a iterative procedure. The initial values for the eleven transformation coefficients  $L_1 \dots L_{11}$  in this iterative procedure, can be calculated disregarding the terms  $x'K_1 r^2$  e  $y'K_1 r^2$  and resolving the remaining eleven linear equations according to what was previously described. The initial value for  $K_1$  can be considered to be zero.

The traditional parameters of the interior and external orientation are included in the coefficient D.L.T.  $L_1 \dots L_{11}$  and can be expressed as follows:

$$\begin{aligned}
 \omega &= \tan^{-1} \frac{-L_{10}}{L_{11}} \\
 m_{11} &= \frac{L(x_p L_9 - L_1)}{c_x} \\
 \kappa &= \frac{\cos^{-1} m_{11}}{\cos f} \\
 LL &= \begin{bmatrix} L_1 & L_2 & L_3 \\ L_5 & L_6 & L_7 \\ L_9 & L_{10} & L_{11} \end{bmatrix} \\
 \begin{bmatrix} X_c \\ Y_c \\ Z_c \end{bmatrix} &= LL^{-1} \begin{bmatrix} L_4 \\ L_8 \\ 1 \end{bmatrix}
 \end{aligned}$$

#### Linearization of the equations

The equations [5] are not linear and cannot be used within the program of calculation; therefore

that have been linearized with using the Taylor's series expansion within and around the approximate values. Assuming:

$$f_1 = x + x'K_1 r^2 = \frac{X}{A} L_1 + \frac{Y}{A} L_2 + \frac{Z}{A} L_3 + \frac{1}{A} L_4 - \frac{xX}{A} L_9 - \frac{yY}{A} L_{10} - \frac{zZ}{A} L_{11}$$

$$f_2 = y + y'K_1 r^2 = \frac{X}{A} L_5 + \frac{Y}{A} L_6 + \frac{Z}{A} L_7 + \frac{1}{A} L_8 - \frac{yY}{A} L_{10} - \frac{zZ}{A} L_{11}$$

where

$$x' = x - x_0$$

$$y' = y - y_0$$

$$r^2 = x'^2 + y'^2$$

$$A = L_9 X + L_{10} Y + L_{11} Z + 1$$

and assuming further

$$B = L_1 X + L_2 Y + L_3 Z + L_4$$

$$C = L_5 X + L_6 Y + L_7 Z + L_8$$

the equations can be written

$$-f_1 l_0 = x + x'K_1 r^2 - \frac{B}{A}$$

$$-f_2 l_0 = y + y'K_1 r^2 - \frac{C}{A}$$

and the coefficients of the  $\Delta$  increments:

$$\frac{\partial f_1}{\partial L_1} = \frac{X}{A}$$

$$\frac{\partial f_1}{\partial L_2} = \frac{Y}{A}$$

$$\frac{\partial f_1}{\partial L_3} = \frac{Z}{A}$$

$$\frac{\partial f_1}{\partial L_4} = \frac{1}{A}$$

$$\frac{\partial f_1}{\partial L_5} = \frac{\partial f_1}{\partial L_6} = \frac{\partial f_1}{\partial L_7} = \frac{\partial f_1}{\partial L_8} = 0$$

$$\frac{\partial f_1}{\partial L_9} = -\frac{L_1 X X}{A^2} - \frac{L_2 Y X}{A^2} - \frac{L_3 Z X}{A^2} +$$

$$-\frac{L_4 X}{A^2} + \frac{xXA - xXL_9 X}{A^2} +$$

$$+ \frac{yXL_{10} X}{A^2} + \frac{zXL_{11} X}{A^2} =$$

$$= -\frac{X}{A^2} (L_1 X + L_2 Y + L_3 Z + L_4) +$$

$$+ \frac{xXA - xXL_9 X}{A^2} + \frac{xX}{A^2} (YL_{10} + ZL_{11} + 1) =$$

$$= -\frac{XB}{A^2} - \frac{xX}{A} +$$

$$+ \frac{xX}{A^2} (L_9 X + L_{10} Y + L_{11} Z + 1) =$$

$$= -\frac{XB}{A^2}$$

$$\frac{\partial f_1}{\partial L_{10}} = \dots = -\frac{YB}{A^2}$$

$$\frac{\partial f_1}{\partial L_{11}} = \dots = -\frac{ZB}{A^2}$$

$$\frac{\partial f_1}{\partial K_1} = -x' r^2$$

analogously for  $f_2$

$$\frac{\partial f_2}{\partial L_1} = \frac{\partial f_2}{\partial L_2} = \frac{\partial f_2}{\partial L_3} = \frac{\partial f_2}{\partial L_4} = 0$$

$$\frac{\partial f_2}{\partial L_5} = \frac{X}{A}$$

$$\frac{\partial f_2}{\partial L_6} = \frac{Y}{A}$$

$$\frac{\partial f_2}{\partial L_7} = \frac{Z}{A}$$

$$\frac{\partial f_2}{\partial L_8} = \frac{1}{A}$$



$$\frac{\partial f_2}{\partial L_9} = - \frac{XC}{A^2}$$

$$\frac{\partial f_2}{\partial L_{10}} = - \frac{YC}{A^2}$$

$$\frac{\partial f_2}{\partial L_{11}} = - \frac{ZC}{A^2}$$

$$\frac{\partial f_2}{\partial K_1} = - y' r^2$$

For every control point it is possible to write two equations of the kind we have just seen; the system formatted by such equations, expressed in matrix form, for  $n$  points, is:

$$A \Delta L = l$$

where:

$$A = \begin{bmatrix} \frac{X_1}{A} & \frac{Y_1}{A} & \frac{Z_1}{A} & \frac{1}{A} & 0 & 0 & 0 & 0 & -\frac{X_1 B}{A^2} & -\frac{Y_1 B}{A^2} & -\frac{Z_1 B}{A^2} & -x_1' r_1^2 \\ 0 & 0 & 0 & 0 & \frac{X_1}{A} & \frac{Y_1}{A} & \frac{Z_1}{A} & \frac{1}{A} & -\frac{X_1 C}{A^2} & -\frac{Y_1 C}{A^2} & -\frac{Z_1 C}{A^2} & -y_1' r_1^2 \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ \frac{X_n}{A} & \frac{Y_n}{A} & \frac{Z_n}{A} & \frac{1}{A} & 0 & 0 & 0 & 0 & -\frac{X_n B}{A^2} & -\frac{Y_n B}{A^2} & -\frac{Z_n B}{A^2} & -x_n' r_n^2 \\ 0 & 0 & 0 & 0 & \frac{X_n}{A} & \frac{Y_n}{A} & \frac{Z_n}{A} & \frac{1}{A} & -\frac{X_n C}{A^2} & -\frac{Y_n C}{A^2} & -\frac{Z_n C}{A^2} & -y_n' r_n^2 \end{bmatrix}$$

$$l = \begin{bmatrix} x_1 + x_1' K_1 r_1^2 - \frac{B}{A} \\ y_1 + y_1' K_1 r_1^2 - \frac{C}{A} \\ \dots \\ \dots \\ x_n + x_n' K_1 r_n^2 - \frac{B}{A} \\ y_n + y_n' K_1 r_n^2 - \frac{C}{A} \end{bmatrix} \quad \Delta L = \begin{bmatrix} DL_1 \\ DL_2 \\ DL_3 \\ DL_4 \\ DL_5 \\ DL_6 \\ DL_7 \\ DL_8 \\ DL_9 \\ DL_{10} \\ DL_{11} \\ DK_1 \end{bmatrix}$$

with  $n > 6$ .

As it has already been said, it is essential to know the approximate initial values of the unknown  $L_1 \dots L_{11}$ ,  $K_1$  for the solution of the system; these values can be arrived at assuming  $K_1 = 0$  and using the direct solution.

At the end of the calculation procedure the program visualizes the value of  $\sigma_0^2$  and those of the residuals of

the equations; it asks the user if the values of  $L$  must be updated adding the values of  $\Delta L$  or if the values of the preceding repetition will be used as definitive values.

The values of  $L_1 \dots L_{11}$ , the calculated value of  $K_1$  and their median squared remainders are shown visually on the monitor; also shown are the traditional parameters of orientation,  $x_c, y_c, f, \omega, \phi, \kappa, X_0, Y_0, Z_0$ .

#### Condition equation on the parameters of the D.L.T.

It is possible to insert into the basic equations:

$$x = \frac{L_1 X + L_2 Y + L_3 Z + L_4}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

$$y = \frac{L_5 X + L_6 Y + L_7 Z + L_8}{L_9 X + L_{10} Y + L_{11} Z + 1}$$

the link that lies between the 11 D.L.T. parameters and the 9 independent parameters necessary for the transformation. That has been realized introducing two condition equations for the 11 parameters. The equations are:

$$(L_1^2 + L_2^2 + L_3^2) - (L_5^2 + L_6^2 + L_7^2) - (C^2 - B^2)/D = 0$$

where

$$A = (L_1 L_5 + L_2 L_6 + L_3 L_7)$$

$$B = (L_1 L_9 + L_2 L_{10} + L_3 L_{11})$$

$$C = (L_5 L_9 + L_6 L_{10} + L_7 L_{11})$$

$$D = (L_9^2 + L_{10}^2 + L_{11}^2)$$

These equations can be used in case the difference in scale should not be modeled and when there is a lack of orthogonality between the axes; in the software such equations have not been utilized in order to allow for the deformations introduced in the scanner that can be corrected with the similar transformation introduced utilizing all 11 parameters.

#### The multi-image restitution

After having calculated the 11 parameters of the D.L.T. and the  $K_1$  term, isolating  $X, Y, Z$ , the pair of [4] equations can be written as follows:

$$x + x' K_1 r^2 - L_4 = X [L_1 - (x + x' K_1 r^2) L_9] +$$

$$+ Y [L_2 - (x + x' K_1 r^2) L_{10}] + Z [L_3 - (x + x' K_1 r^2) L_{11}]$$

$$y + y' K_1 r^2 - L_8 = X [L_5 - (x + x' K_1 r^2) L_9] +$$

$$+ Y [L_6 - (x + x' K_1 r^2) L_{10}] + Z [L_7 - (x + x' K_1 r^2) L_{11}]$$

Writing these equations for the  $n$  images in which the point to plot does appear, the following system is obtained:

$$Ax = l$$

introducing the following terms in order to simplify the notation:

$$R_x = x + x' K_I r^2$$

$$R_y = y + y' K_I r^2$$

achieves:

$$A = \begin{bmatrix} L_{11} - R_{X_1} L_{9_1} & L_{21} - R_{X_1} L_{10_1} & L_{31} - R_{X_1} L_{11_1} \\ L_{5_1} - R_{Y_1} L_{9_1} & L_{6_1} - R_{Y_1} L_{10_1} & L_{7_1} - R_{Y_1} L_{11_1} \\ \dots & \dots & \dots \\ \dots & \dots & \dots \\ L_{1n} - R_{X_n} L_{9_n} & L_{2n} - R_{X_n} L_{10_n} & L_{1n} - R_{X_n} L_{11_n} \\ L_{1n} - R_{X_n} L_{9_n} & L_{6n} - R_{Y_n} L_{10_n} & L_{7n} - R_{Y_n} L_{11_n} \end{bmatrix}$$

$$l = \begin{bmatrix} R_{x1} - L_{4_1} \\ R_{y1} - L_{8_1} \\ \dots \\ \dots \\ R_{xn} - L_{4_n} \\ R_{yn} - L_{8_n} \end{bmatrix} \quad x = \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}$$

This system always has a lesser number of unknowns than that of the equations and therefore is resolved using the method of least squares.

At the end of the calculations the program provides:

- the estimated  $X, Y, Z$  coordinates which AutoCAD reads and utilizes for the restitution;
- the residual errors of the equations,  $s_0^2$ , and the standard deviation of  $X, Y$  e  $Z$ .

### Limits of the D.L.T

Having already listed the advantages to using the D.L.T. now some of its main disadvantages must be indicate.

First and foremost, the D.L.T. needs at least 6 three dimensional control points in order to estimate the parameters: this involves an increase in the topographic work which, however, in the case of a strictly didactic exercise could be considered negligible. Another negative factor (which is common to many photogrammetric applications), is the fact that the D.L.T. is very sensitive to the spatial distribution of the control points. A situation to be avoided is where all of the control points lie on a plane or are next to one another. In this case the solution becomes unstable due to the poor conditioning of the normal system. The points therefore must have a distribution that is the most varied possible compatibly with the depth the field of the photogram. Moreover, the control points should be positioned around the object to plot. This aspect is

very important from a didactic point of view, in so far as it involves a particular attention to the geometric configuration of the survey on the part of the students. The indication of the value of the determinant of the normal matrix, carried over on the screen of the results of the orientation calculation, provides an index of the geometric configuration linked to the conditioning of the system.

### What it will do

NM3-digit was realized as a "development instrument" where it is possible to experiment with algorithms and impose new applications.

The availability of the source code in Pascal that can be had upon request allows for the writing of new forms of the program.

In particular, the software could evolve itself according to the probable lines of development that are listed below:

- calculate the epipolar plane of every point plotted and show the outline of the image;
- allow for auto correlation

Even the part of the calculation could be the object of experimentation, directed at improving the characteristics: other algorithms of the calculation could be used, as an alternative to the D.L.T., classic collinear equations, in order to make use of, for example, photcameras.

Compared with the D.L.T. condition equations could also be inserted, in order to reduce the instability of the system; the possibilities are: define the condition equations on the object, give the opportunity to ponder an indicative value of the main distance and of the set point, introduce pass points.

But the most substantial additions to the program, in order to bring it closer to the more expensive software, is the integration of adjunctive software directly within the principle code to allow it to execute: the aerial triangulation, the automatic generation of the D.T.M., the normalization of the photographs, the rectification of the photographs, the orthophoto, and the projection of the images onto non-planar surfaces.

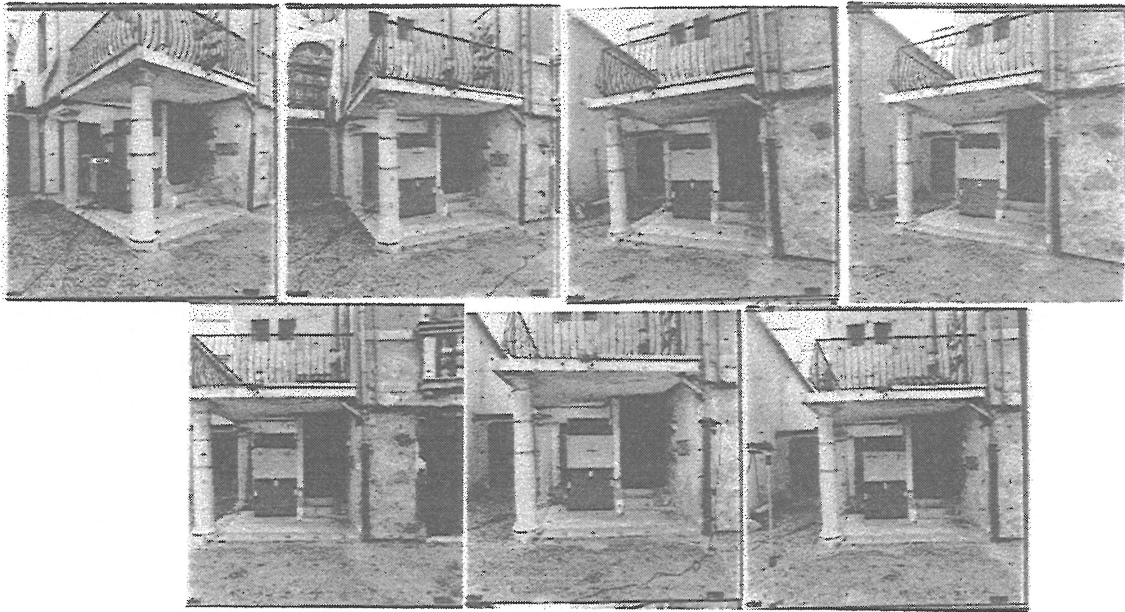
### The authors

The authors of this paper have occupied themselves in the development of the analytical part and the designing of the software, based on the didactic experiences carried out in the courses of Professor Clemente di Thiene and Carlo Monti. The NM3-Digit has been written by Francesco Guerra and Eugenio Mario for the graduating thesis of the latter. In particular, Francesco Guerra oversaw the design of the numeric calculation and Eugenio Mario took care of the graphic interface.

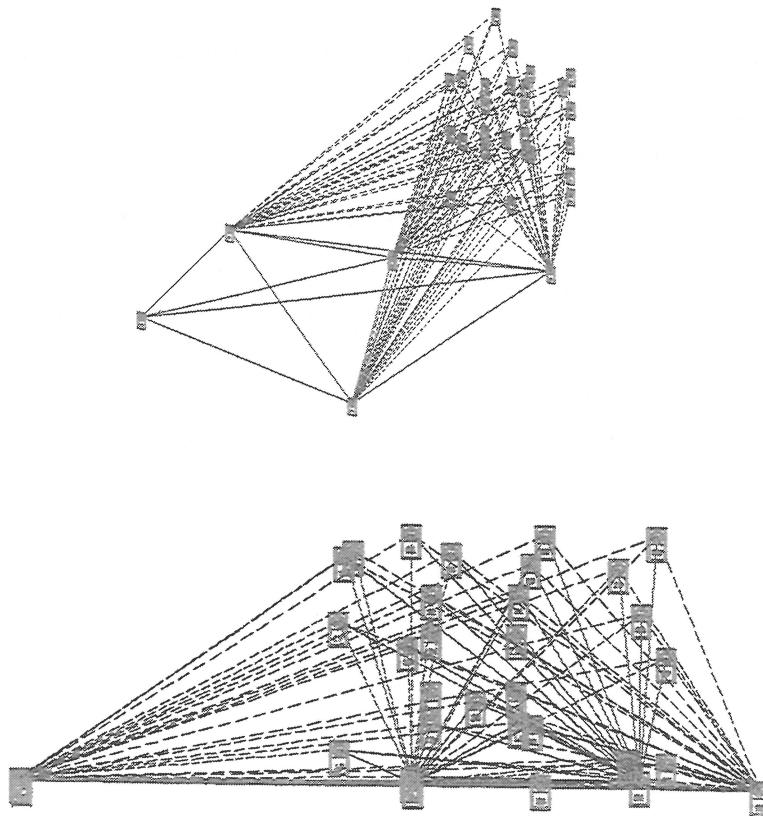
**Laboratory test**

The first test was done using 7 images oriented with 23 control points surveyed with angles and distances from 4 stations. The images are scanned camera Rollei 6006 photographs.

The restitution accuracy are shown in the next tables where can be read the topographi coordinates, the photogrammetric coordinates and their differences.



*Fig. 1. Images*



*Fig. 2. The topographic net*

Point	Topographic coordinates			Photogrammetric coordinates			Differences		
	X (m)	Y (m)	Z (m)	X (m)	Y (m)	Z (m)	$\Delta x$ (m)	$\Delta y$ (m)	$\Delta z$ (m)
1	3,978790	3,538196	2,524979	3,980104	3,535950	2,522782	-0,001314	0,002246	0,002197
2	6,340784	3,898351	2,522043	6,339027	3,905748	2,518710	0,001757	-0,007397	0,003333
3	6,497713	4,203215	2,518584	6,498951	4,209677	2,521002	-0,001238	-0,006462	-0,002418
4	3,973667	3,655477	0,026720	3,974153	3,655190	0,026537	-0,000486	0,000287	0,000183
5	6,605795	4,447138	0,172297	6,606476	4,450539	0,170592	-0,000681	-0,003401	0,001705
6	3,947624	3,713668	1,368121	3,947215	3,714857	1,370303	0,000409	-0,001189	-0,002182
7	6,597227	4,409111	1,266480	6,598841	4,417929	1,267077	0,000386	-0,008818	-0,000597
8	6,333075	5,122012	1,715597	6,334065	5,122827	1,716937	-0,000990	-0,000815	-0,001340
9	5,213523	5,390890	0,559818	5,214445	5,394856	0,558153	-0,000922	-0,003866	0,001665
11	5,081204	5,448670	1,898871	5,081162	5,454173	1,902543	0,000042	-0,004503	-0,002572
12	4,180128	5,199926	1,894403	4,187728	5,202873	1,895807	0,002400	-0,002947	-0,001204
13	4,186075	5,203496	0,574225	4,187086	5,205615	0,574249	-0,001011	-0,002119	-0,000024
14	5,079735	5,454494	0,588865	5,078818	5,450538	0,587850	0,000917	0,003956	0,002015
21	6,196828	5,448353	0,216831	6,195087	5,453011	0,216030	0,001741	-0,004658	0,000801
22	4,645674	5,328887	0,802078	4,649520	5,327522	0,800508	-0,003846	0,001165	0,001570

Fig. 3. Topographical and photogrammetrical comparison

The table underlines the software is able to execute right orientation and restitution. But it's important to understand that the test condition are particular:

- high accuracy of control points;
- optimal distribution of control points related to D.L.T.;
- marked points are collimated.

These are not the practical condition of an architectural survey: in fact the accuracy is worse.



### The survey of the facade of Villa Della Torre Chapel

This is a practical example. The surveyed object is the principle facade of Villa Della Torre in Fumane (VR) designed by Michele Sammicheli.

### Images

The photogrammetrical model is obtained scanning 3 images (Rollei 6006m camera)

The 12 control points have a uniform distribution on the facade plane.



Fig. 4. Image1, Image2, Image3

### Restitution



Fig.5. Vectorial drawing from the restituted individual points

## Orientation

The orientation parameters are shown in a window where even the D.L.T. parameters are contained

Calcolo dell'Orientamento Foto1

Nome pt.	X lastra	Y lastra	res. equaz.	res. equaz.2	res. stand.1	res. stand.2	param	valore	s-g.m.
1	349	315	-0,331328	0,269339	-0,930708	0,585632	L1	92,089265	0,744071
2	647	342	0,671842	-0,349778	1,029945	-0,598268	L2	7,271868	0,289992
							L3	-17,513372	6,721845
							L4	1474,657804	13,905643
							L5	30,145064	0,321604
							L6	-65,420312	0,894870
							L7	-44,920712	4,318402
							L8	295,073879	8,669929
							L9	0,044238	0,000579
							L10	0,010325	0,000444
							L11	-0,072900	0,009259
							K1	0,000000	0,000000

Eventuali messaggi d'errore

Determinante matrice normale  
1,21523880377392545

Orientamento Esterno		Orientamento Interno	
Xp	-15,348239	Xo	735,566234
Yp	3,274529	Yo	532,929285
Zp	4,856955	Cx	810,180276
Om	8,957152	Cy	831,960875
Ri	34,474956	C	821,070575
Ka	-4,341941		

Signazero fix precedente: 0,330765

Signazero attuale: 0,330765

Soluzione diretta  Approssimato

Soluzione iterativa  Orientamento

Memorizza file \*.par

Torna coord. lastra

Fig. 6. Image 1 orientation.

Calcolo dell'Orientamento Foto2

Nome pt.	X lastra	Y lastra	res. equaz.	res. equaz.2	res. stand.1	res. stand.2	param	valore	s-g.m.
1	385	634	0,027397	0,304052	0,061895	1,496710	L1	99,814364	1,740848
2	535	665	-0,055446	-0,792340	-0,089700	-1,230659	L2	-1,088523	0,385226
							L3	-63,990861	11,067764
							L4	1734,122180	36,527200
							L5	5,976997	0,823828
							L6	-90,783482	2,629936
							L7	-61,134391	6,843623
							L8	798,566666	15,885516
							L9	0,014230	0,002097
							L10	0,000336	0,000676
							L11	-0,123590	0,017359
							K1	0,000000	0,000000

Eventuali messaggi d'errore

Determinante matrice normale  
5,47816591791439E38

Orientamento Esterno		Orientamento Interno	
Xp	-13,109562	Xo	602,733483
Yp	3,494577	Yo	491,701487
Zp	6,591396	Cx	738,298620
Om	0,173212	Cy	731,109307
Ri	7,297527	C	734,703964
Ka	-0,875167		

Signazero fix precedente: 0,204934

Signazero attuale: 0,204934

Soluzione diretta  Approssimato

Soluzione iterativa  Orientamento

Memorizza file \*.par

Torna coord. lastra

Fig. 7. Image 2 orientation.

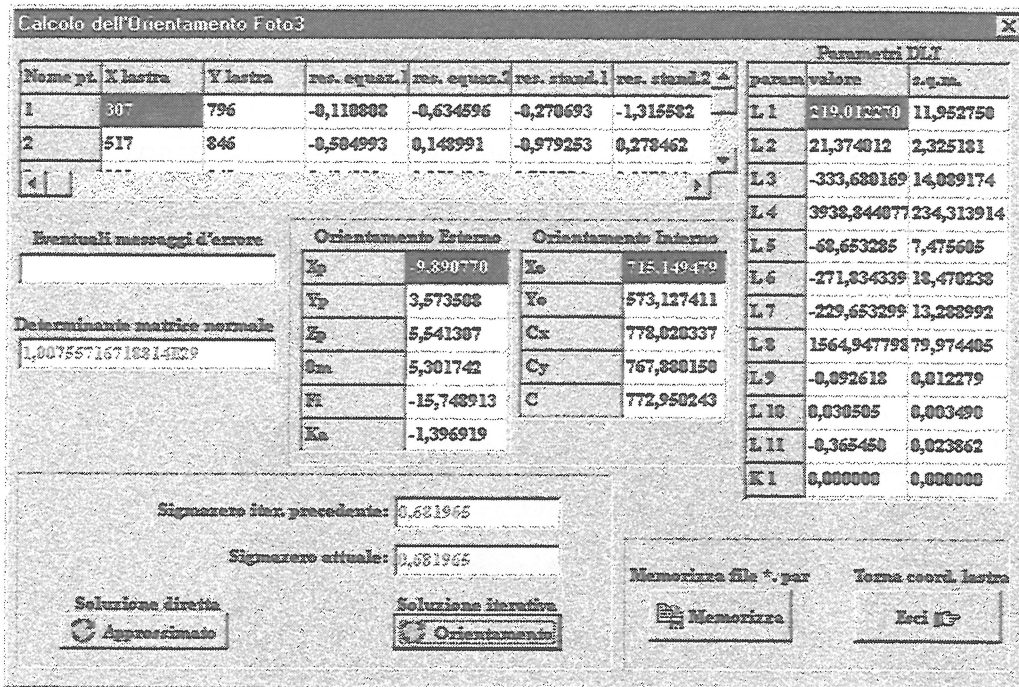


Fig. 8. Image 3 orientation.

Numerical restitution

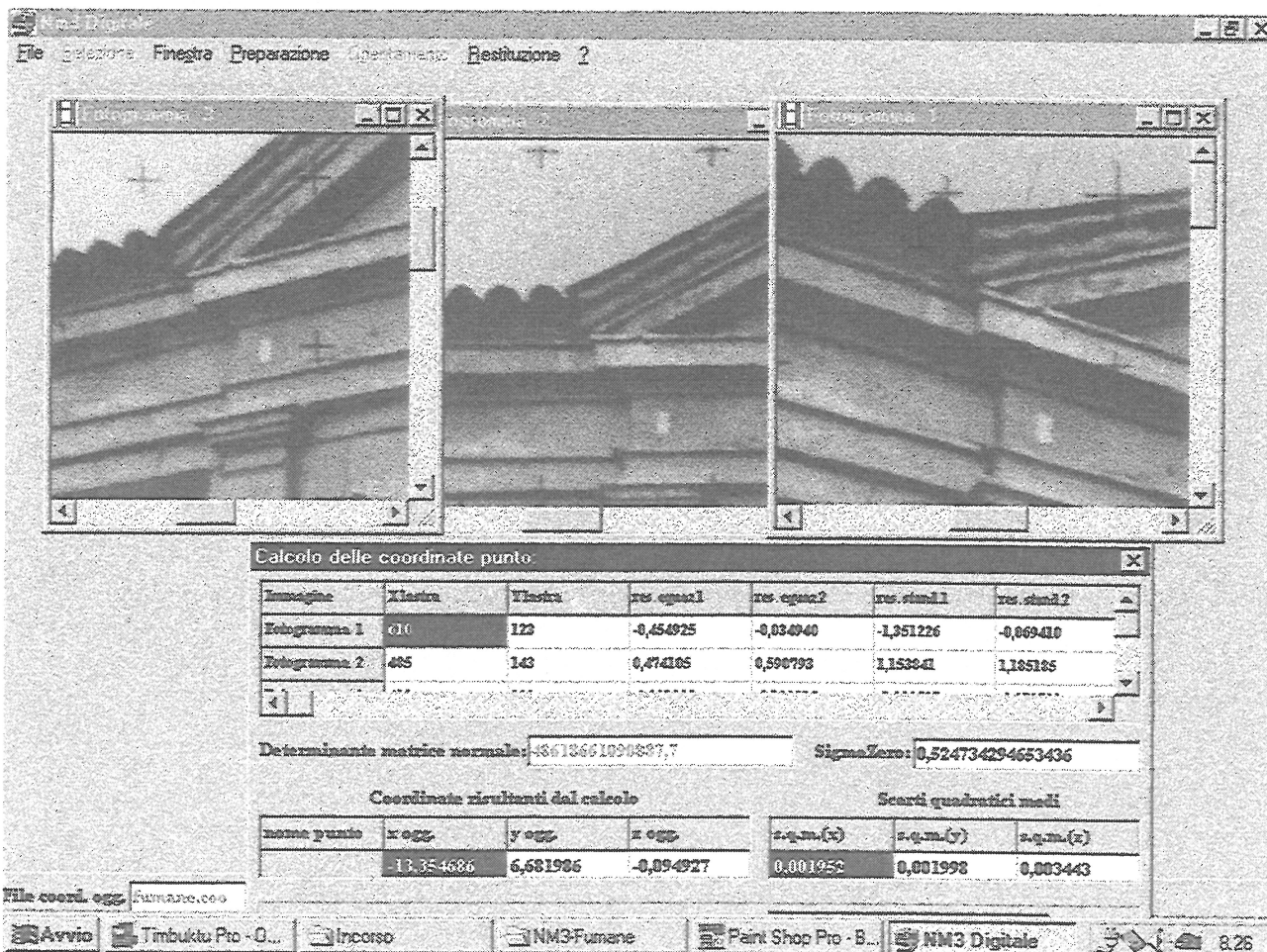


Fig. 9. Numerical restitution window.



### Deformed images test

The scanned image are modified to introduce geometrical deformation. These deformation are:

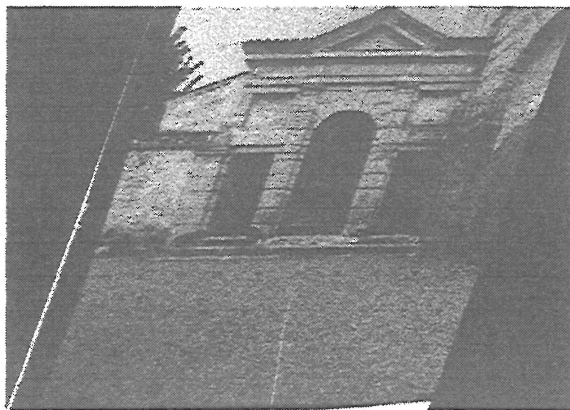
- a different scale in x and y axes,
- a shear between x and y axes.

The aim is to test the algorithm, modelling the deformation, that allows to orient the images guaranteing a right restitution.

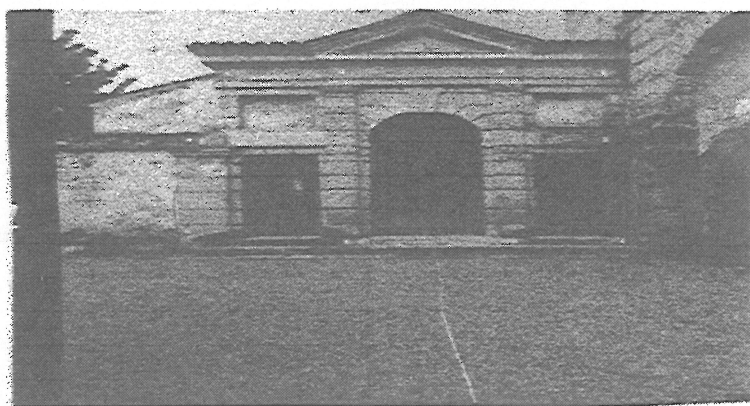
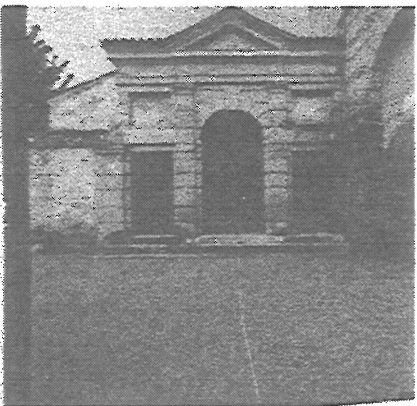
Original and deformed images had been oriented with the same control points. Then the same points had been restituted from the 2 set of images. The coordinates comparison underlines it's possible to have a right restitution starting from deformed images, and the collimation differences are caused by casual errors.

### Deformation

Image 2: deformation exemple.



*Fig. 10. Shear between axes: case A.*



*Fig. 11. Different scale in x and y axes: case B.*



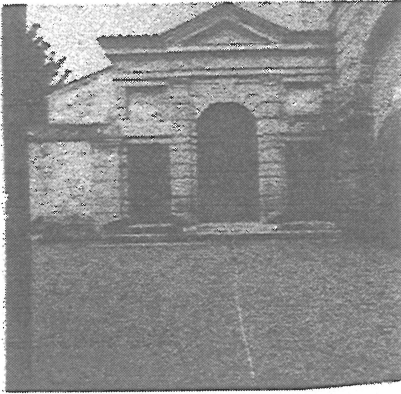


Fig. 12. Both above-mentioned deformations: case C.

Deformed images orientation.

Calcolo dell'Orientamento Foto2

Nome pt.	X lastra	Y lastra	res. equaz. 1	res. equaz. 2	res. stand. 1	res. stand. 2	Parametri DLT		
							param.	valore	s.g.m.
1	363	444	-0,151982	-0,266066	-0,416219	-0,469398	L 1	122,21865	1,782245
2	681	464	0,132330	-0,074457	0,254938	-0,113977	L 2	-1,140694	0,402243
							L 3	-91,319994	11,105830
							L 4	2220,282485	37,224062
							L 5	4,718858	0,622949
							L 6	-63,306159	1,436093
							L 7	-47,926623	5,286617
							L 8	563,570380	10,192154
							L 9	0,014307	0,001576
							L 10	0,000772	0,000559
							L 11	-0,123577	0,014102
							K 1	0,000000	0,000000

Eventuali messaggi d'errore

Determinante matrice normale  
2,29749153521129E39

Orientamento Esterno		Orientamento Esterno	
Xp	12,548614	Xo	347,643769
Yp	2,926666	Yo	383,891136
Zp	6,657662	Cx	939,514672
Om	0,397536	Cy	511,308443
Fi	7,337410	C	725,411558
Ka	-0,931933		

Signazero fix. precedente: 0,779445

Signazero attuale: 0,779445

Soluzione diretta  Approssimato

Soluzione iterativa  Orientamento

Memorizza file \*.par

Torna coord. lastra

Fig. 13. Deformed image 2 (caso B).

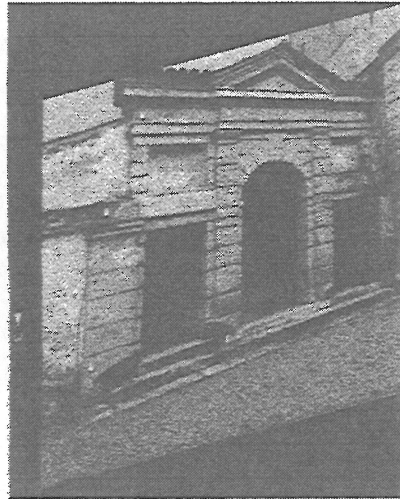
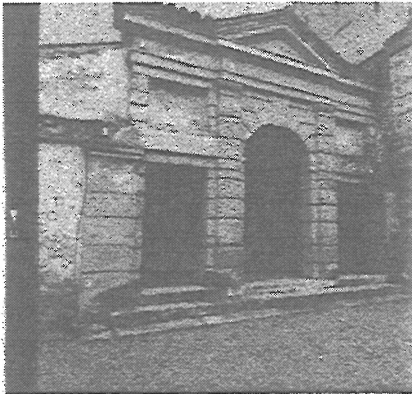


Fig. 14. Image 1: the original and the deformed one ( caso C).

Calcolo dell'Orientamento Foto 1

Nome pt.	X lastra	Y lastra	res. equaz. 1	res. equaz. 2	res. stand. 1	res. stand. 2	Parametri DEL		
							param.	valore	s.g.m.
1	249	1064	-0,573298	-0,394327	-1,650177	-0,952314	L1	91,874868	0,695762
2	648	983	0,178173	0,290441	0,303059	0,521090	L2	7,317538	0,269800
							L3	-14,595006	6,705791
							L4	1472,005585	13,100475
							L5	20,272629	0,452953
							L6	-64,088277	0,833103
							L7	-67,270932	5,034201
							L8	824,506335	5,707695
							L9	0,044323	0,000559
							L10	0,010347	0,000400
							L11	-0,070638	0,009077
							K1	0,000000	0,000000

Eventuali messaggi d'errore

Determinante matrice normale  
1,914279131560245

Orientamento Esterno		Orientamento Interno	
Xp	15,477091	Xo	733,414081
Yp	2,863089	Yo	706,282242
Zp	4,864724	Cx	833,811752
Sm	9,259674	Cy	884,252800
H	35,378948	C	859,032276
Ka	-4,660611		

Segnare iter precedente: 0,808306

Segnare attuale: 0,808306

Soluzione diretta  Approssimato

Soluzione iterativa  Orientamento

Memorizza file \*.par

Torna coord. lastra

Fig. 15. Deformed image 1 ( caso C).

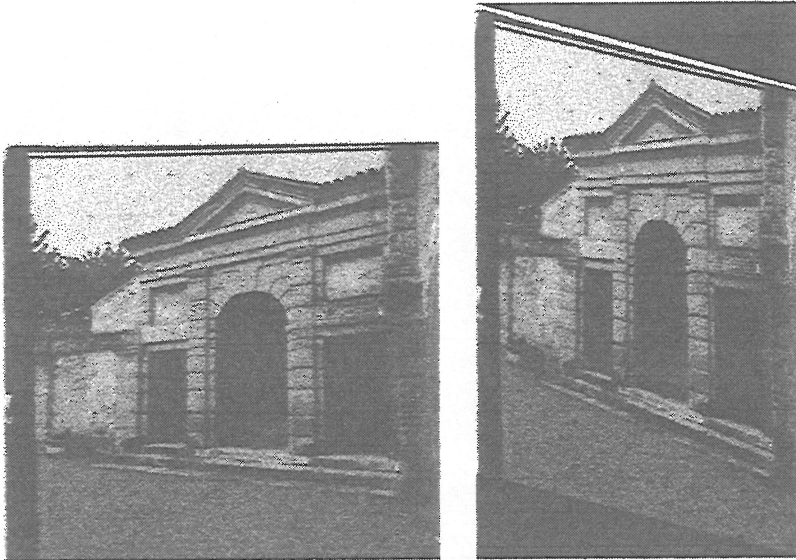


Fig. 16. Image 3: the original and the deformed one (case C).

Calcolo dell'Orientamento Foto3

Nome pt.	X lastra	Y lastra	res. equaz.1	res. equaz.2	res. stand.1	res. stand.2	param.	valore	c.g.m.
1	307	796	-0,110835	-0,634604	-0,270684	-1,315594	L 1	219,012135	11,952713
2	517	846	-0,504995	0,148999	-0,979253	0,278478	L 2	21,374062	2,325191
							L 3	-333,638149	14,689169
							L 4	3938,840493	234,312971
							L 5	-68,653164	7,475575
							L 6	-271,833952	18,470137
							L 7	-229,652856	13,289030
							L 8	1564,946189	79,973982
							L 9	-0,092618	0,012279
							L 10	0,030505	0,003490
							L 11	-0,365450	0,023362
							K 1	0,000000	0,000000

Orientamento Esterno		Orientamento Interno	
Xp	9,390763	Xo	15,150340
Yp	3,573515	Yo	573,126398
Zp	5,541303	Cx	778,020010
Om	5,301757	Cy	767,879594
Ei	-15,748878	C	772,949802
Ka	-1,396926		

Eventuali messaggi d'errore

Determinante matrice normale  
1,0076440428919E29

Signazero itaz. precedente: 0,681972

Signazero attuale: 0,681967

Soluzione diretta  **Approssimato**

Soluzione iterativa  **Orientamento**

Memorizza file \*.par  **Memorizza**

Torna coord. lastra  **Esci**

Fig. 17. Deformed image 3 (caso C)..

Deformed image restitution:

Calcolo delle coordinate punto

Immagine	X sinistra	Y sinistra	res. eq. x1	res. eq. x2	res. std.1	res. std.2
Fotogramma 1	611	274	0,279285	-1,125658	0,472099	-1,213800
Fotogramma 2	618	109	-0,775600	-0,782158	-1,036354	-0,827957

Determinante matrice normale: 93485625388620,4      SigmaZero: 0,957224925400867

Coordinate risultanti dal calcolo			Scarti quadratici medi			
nome punto	x ogg.	y ogg.	z ogg.	s.q.m.(x)	s.q.m.(y)	s.q.m.(z)
	11,349247	6,682277	-0,085407	0,006033	0,006125	0,012651

Directory dove è stato salvato il file PUNTO.SOL: C:\INCORSO\tracce\NM3-Fumane

File coord. ogg.    Aziona:    Specifica il file dove salvare il punto    Aggiungi il punto al file    Torna coord. sinistra

Avvio    Timbuktu Pro - 0...    Incorso    NM3-Fumane    Paint Shop Pro    NM3 Digitale    8.45

Fig. 18. deformed images numerical restitution. The restituted point is the same of fig.9.

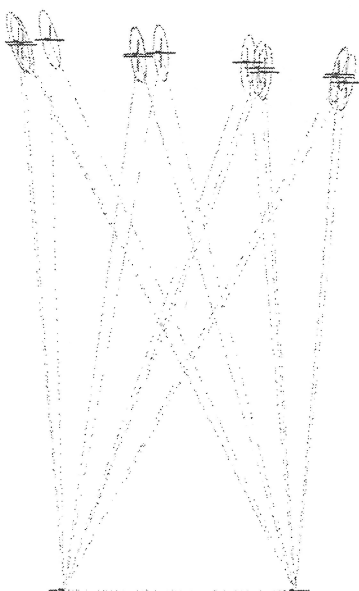


Fig. 19. Image control points scheme.